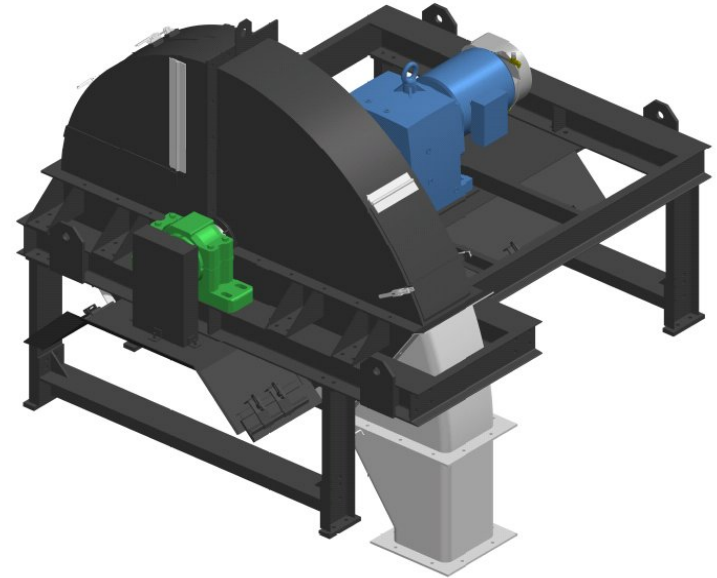


SGS MECHANICAL SAMPLING SYSTEMS

WHEN YOU NEED TO BE SURE



- SGS has manufactured and supplied mechanical sampling equipment (MSS) primarily in Australia, Asia, and Europe for over 20 years. SGS cross-belt samplers are re-engineered and the design significantly updated and improved supply superior, yet cost effective systems.

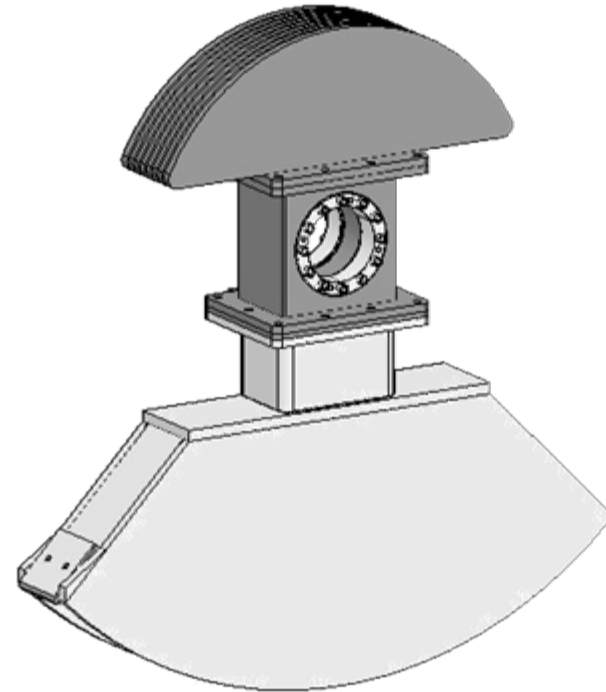


CROSS BELT SAMPLER DESIGN FEATURES

- Available to fit any size, speed or capacity belt, metric or imperial
- Large range of top sizes can be accommodated
- Heavy duty cutter and enclosure construction
- Detailed engineering of mechanical components
- Direct drive
- Fluid shear brake
- Adjustable skirt-boards
- Non-stick spiral enclosure
- Closed loop speed and position control available
- Hydraulic drive options available

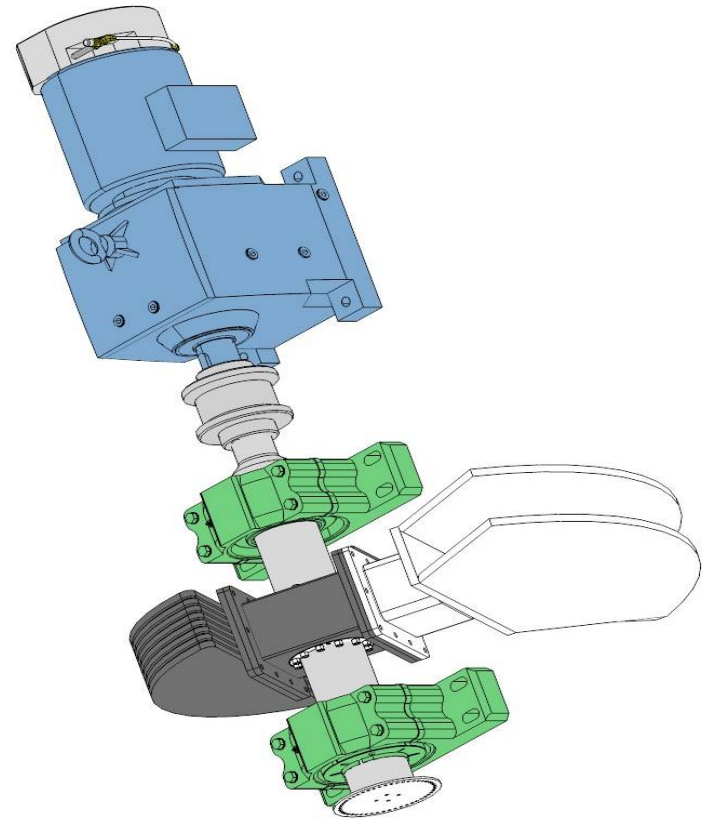
HEAVY DUTY CUTTER

- Ultra heavy duty components for long life
- Engineered to minimize weight without compromising sample integrity
- Engineered to accommodate worst case loading
- Conservative safety factors
- Standard stainless steel cutter body
- Counterweighted for balance and increased inertia
- Counterweight eliminates the forces on the customer's structure resulting from an eccentric cutter load if no counter weight is used
- Belt wiper ensures complete increment collection



CAREFULLY SIZED COMPONENTS

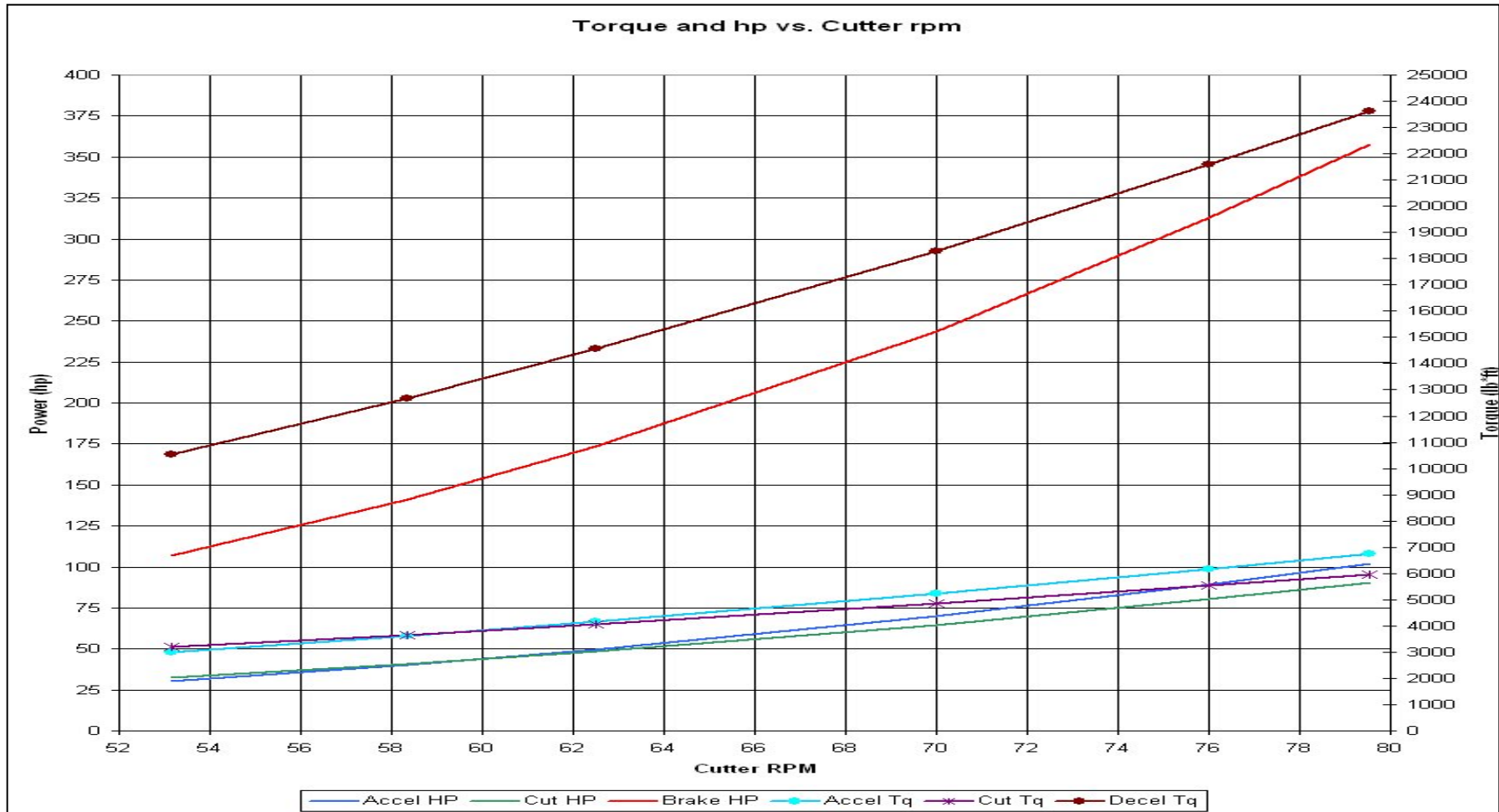
- Drive components custom selected for each application
- All components selected for durability
- Components are oversized to handle the harshest conditions
- Shock loading and fatigue are primary design considerations



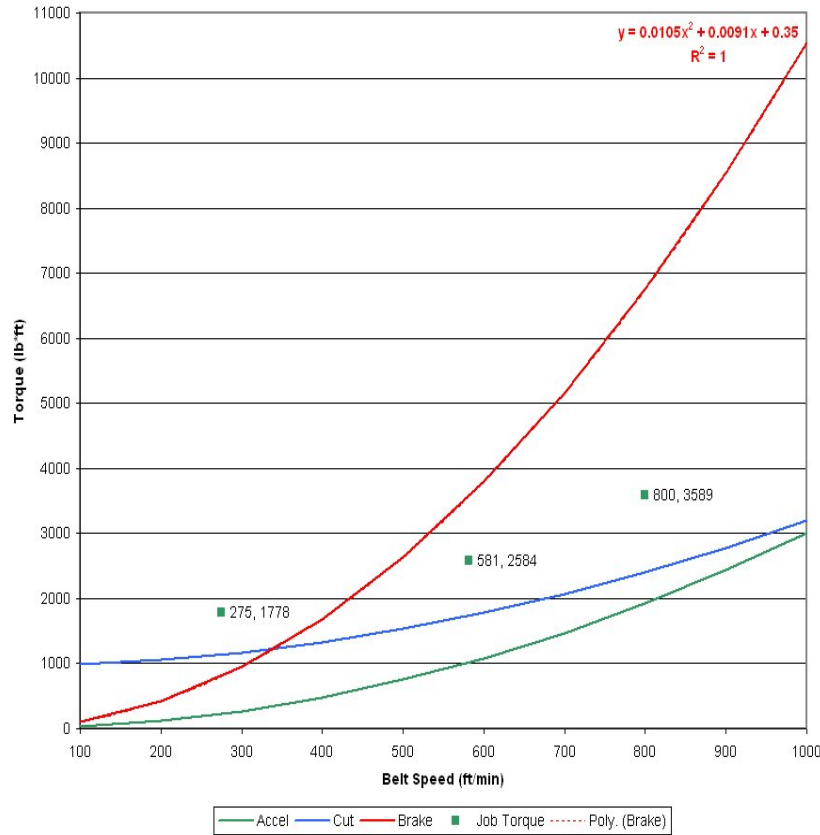


DYNAMIC ANALYSIS

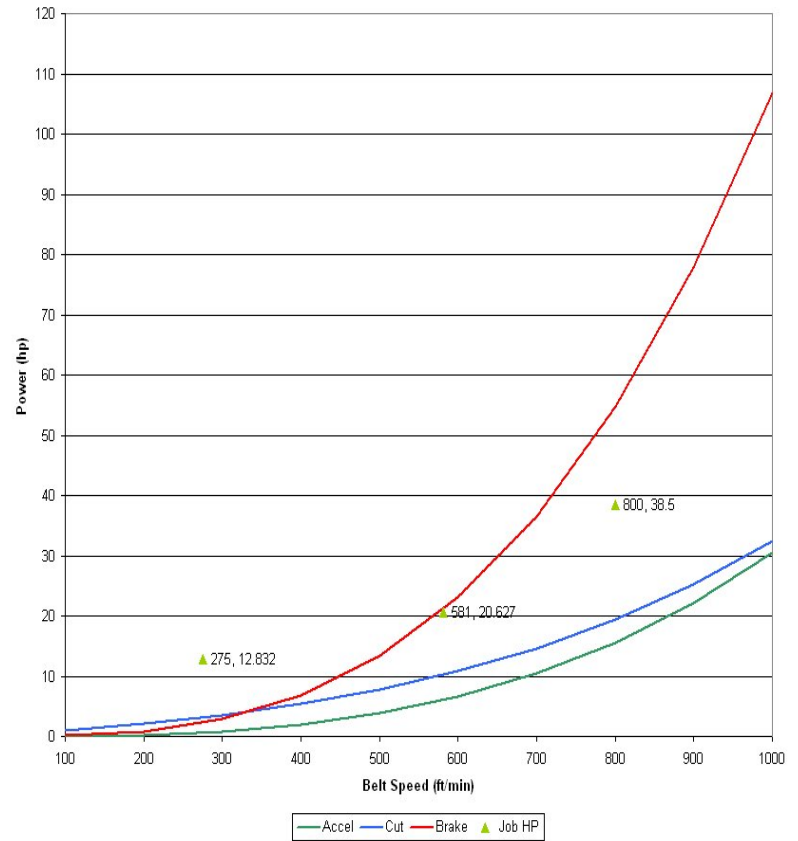
A	B	C	D	E	F	G	H	I	J	K	L	M	N	O
1	Generic 48in Primary		8/17/2009											
2														
3	English/Imperial Units													
4			= Calculated cells											
5		Number	= Input cells											
6	Belt and Material Data		Inputs	Geometric Results			Motion, Torque, and Power							
9	Belt Width (b)	48 in		Cutter Radius (r_c)	27.751 in			Total Cycle Time (estimated)	0.591 s					
10	Belt Capacity	2574 t/hr		Cutter Angle (α_c)	89.3 deg			Minimum Tip Speed of Cutter (min 1.5x of belt speed)	1200.000 ft/min					
11	Belt Speed	800 ft/m		Clearance Radius (r_{cl})	10.789 in			Actual Max Tip Speed of Cutter	1243.771 ft/min		greens ok, reds check gear ratio			
12	Angle Of Idler (β)	35 degrees		Cutter Inside Width (w_{ci})	6 in			Full Speed RPM of cutter (gearbox output)	85.597 RPM					
13	Roller Width plus air gap between rollers (l)	17.5 in		Cutter Outside Width (w_{co})	13 in			Full Speed Angular Velocity	8.964 radians/s		ω = 2π * rev/min			
14	Conveyor Incline Angle	0 degrees		Overall Shaft Length	27.418 in									
15	(if positive material is ascending)			Shaft Dia	4 in									
17	Bulk Material Characteristics			Acceleration Phase (ω₁ - ω₂)										
18	Surcharge Angle (α)	25 degrees		Total Rotational Mass				Acceleration angle in radians	1.169 radians		θ			
19	Nominal Top Size	2 in		Cutter Rotating Mass	902.19 lb			Angular Acceleration	34.355 radians/s ²		α = (ω ₂ ² - ω ₁ ²) / (2θ)			
20	ASTM Factor	1.5 :1		Motor Rotor Mass	0.25 lb			Time to accelerate to full speed	0.261 s		t = (ω ₂ - ω ₁) / α			
22	Construction Materials			Motor Rotating Mass	1.00 lb			Acceleration Torque at main shaft	1228.676 lb*ft		τ = Iα (convert lbm to lb!!!)			14744.1171
23	Cutter			Coupling Rotating Mass	99.88 lb			Acceleration HP	20.032 hp		Hp = (τ * RPM) / 5250			
24	Cutter Side Material Thickness	0.75 in		Total	903.44 lb									
25	Steel Density (304 SS)	0.289 lb/in ³						Constant Speed Phase (ω₂)						
27	Other Parts (hub, counterweight, spacer)			Inertia				Ratio of Cutter tip speed to Belt speed	1.555 :1		Must be greater than 1.5			
28	Thickness	0.5 in		Cutter	1149.618 lb*ft ²			Weight of sample	53.625 lbm					
29	Density (304 SS)	0.289 lb/in ³		Motor (rotor and geartrain)	0.500 lb*ft ²			Angle over which sample is out (out angle - cutter angle)	1.559 radians					
31	Motion Characteristics			Brake	0.061 lb*ft ²			Time to sweep coal off belt	0.174 s					
32	Angle to accelerate cutter to full speed	67.000 degrees		Coupling	0.050 lb*ft ²			Sample CG loc in y-axis (approx)	-21.646 in					
33	Stopping angle	40.000 degrees		Shaft	1.383 lb*ft ²			Velocity of CG of sample @ ω ₂	970.141 ft/min		16.169 ft/s		v = d/t	
34	Overlap between sample out and decel	0.000 degrees		Total Rotational Inertia	1151.612 lb*ft ²			Acceleration of sample	185.879 ft/s ²		a = v/t		Using t/2 because the entire sam	
35	Angle over which sample is out	89.349 degrees		Cutter Rotating Mass	902.19 lb			Mass of coal buildup on cutter side	248.782 lbm				Using t/2 because the entire build	
36	Steady State Angle (pre cut)	163.651 degrees						Deceleration of built up coal	153.280 ft/s ²					
37	Gear Reduction ratio	20.620 to 1		Bearing Reaction Forces				Friction of built up coal on belt	124.391 lbf					
38	Drive RPM from Motor	1765.000 RPM		R _{1x}	0.00 lbf			Force of Coal buildup on cutter side	1308.656 lbf					
40	Component Friction Coefficients			R _{1y}	841.40 lbf			Torque to accelerate sample						
41	Friction Coefficient coal against the cutter α	1.000		R _{2x}	-1433.05 lbf			Friction of coal to walls of cutter	53.625 lbs					F = ma = (W/t/32.2) * a
42	Friction Coefficient coal sliding on the belt α	0.500		R _{2y}	-1743.59 lbf			Friction of sample sliding on the belt	26.813 lbs					
43	Wiper Friction	5.000 lbs/in of wiper						Friction from the cutter wiper	30.000 lbs					
46	Shaft Physical Parameters							Torque due to friction						
47	Bearing Width	1.000 in						hp to accelerate sample	13.268 hp					
48	Driven Stub Shaft	3.000 in						Torque to accelerate and cut the sample	813.794 lb*ft					9765.53 lb*in
49	Driving Stub Shaft	10.000 in												
50	Material Density	0.289 lb/in ³						Braking Phase (ω₂ - ω₁)						
51	σ _u	73200 psi						Stopping arc in radians	0.630 radians		θ			
52	σ _y	31200 psi						Angular deceleration	57.544 radians/s ²		α = (ω ₂ ² - ω ₁ ²) / (2θ)			
53	E (Modulus of Elasticity)	28,500,000						Time to decelerate cutter	0.156 sec		t = (ω ₂ - ω ₁) / α			
54	Torsional Modulus G	11,500,000						Torque to decelerate rotational components						
55	Permissible axial deflection	0.0015 radians						hp to decelerate	2058.033 hp					24696.396 lb*
56	Maximum torsional deflection	0.08 degrees/ft of shaft							33.554 hp					99.808 lb
57	Shaft from motor to cutter							Max Full Cycle Torque						
								Max Full Cycle Torque at Motor shaft	2058.033 lb*ft					24696.396 in*lb
									99.808 lb*ft					1197.691 in*lb
								Ke per stop						
									1436.778 lb*ft					
								Max Power						
									33.554 hp					



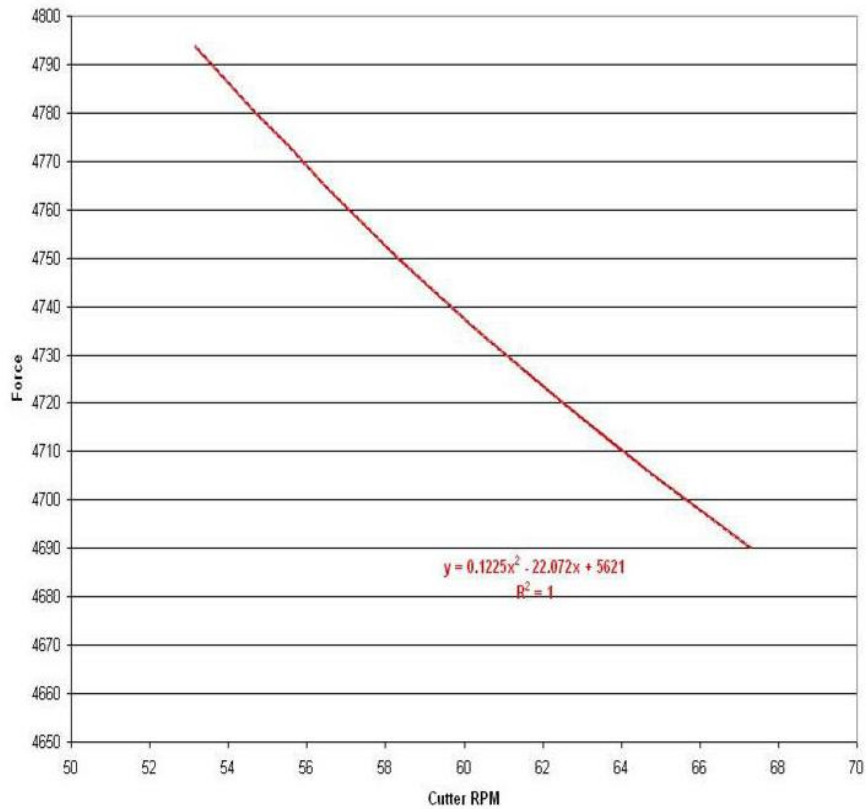
Belt Speed vs. Torque, 72"



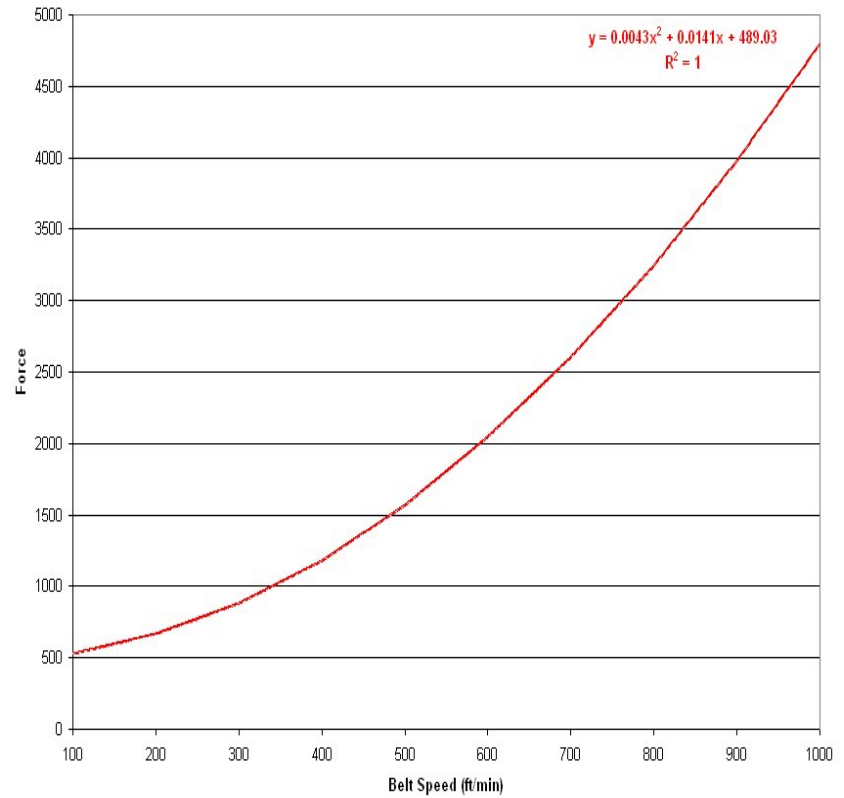
Belt Speed vs. hp



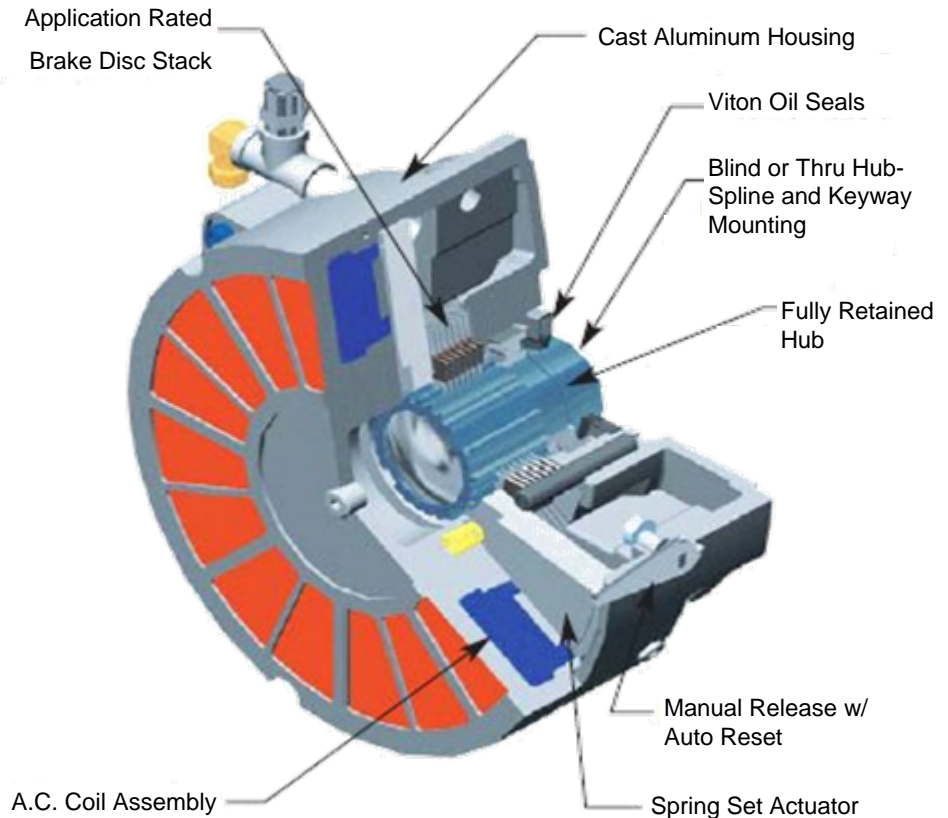
Force on Cutter Due to Coal Buildup vs. Cutter RPM



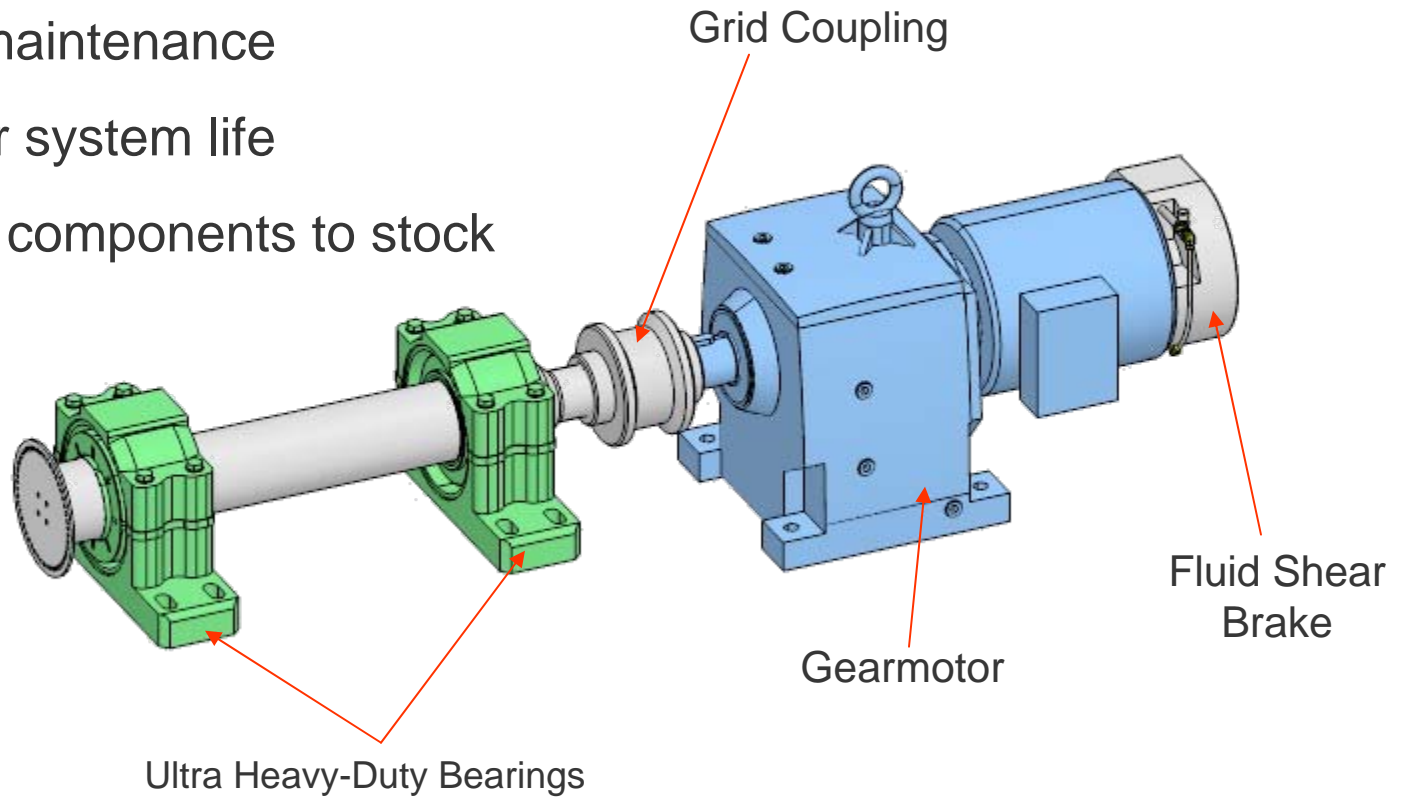
Force on Cutter Due to Coal Buildup

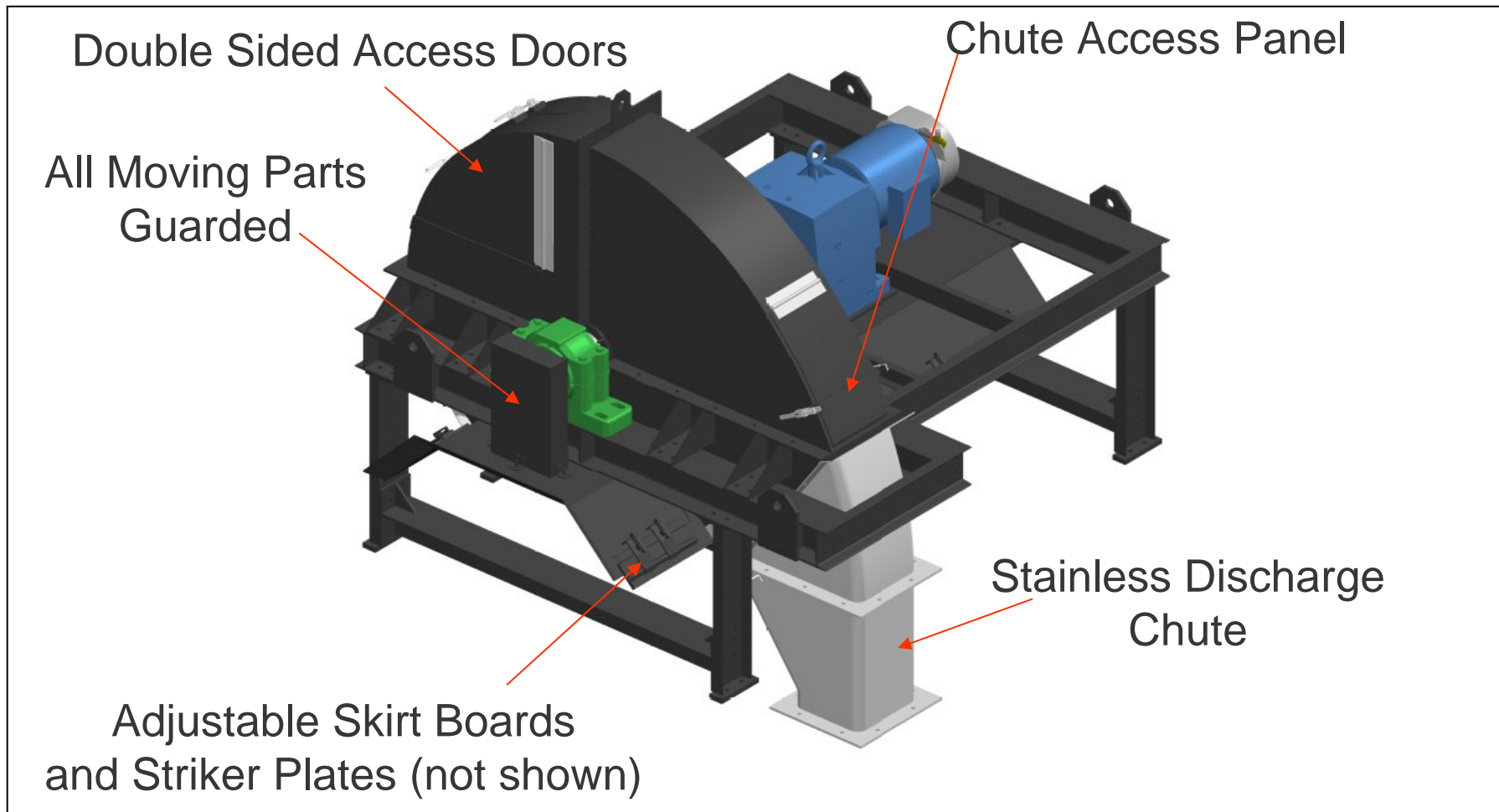


- Nearly eliminates brake maintenance
- Superior stopping capability and response time (<10ms!)
- Potted electric components for superior durability



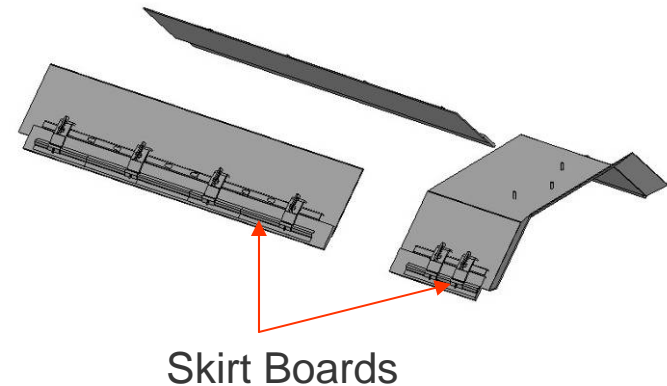
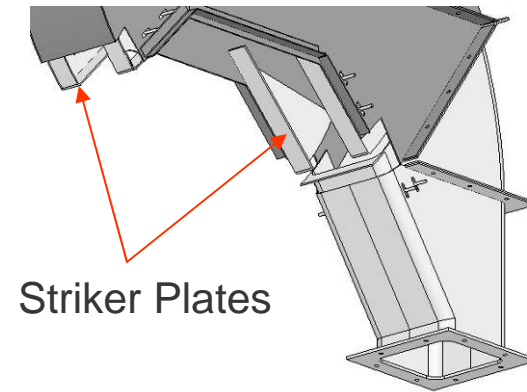
- Direct drive eliminates the clutch-brake
- Less maintenance
- Longer system life
- Fewer components to stock

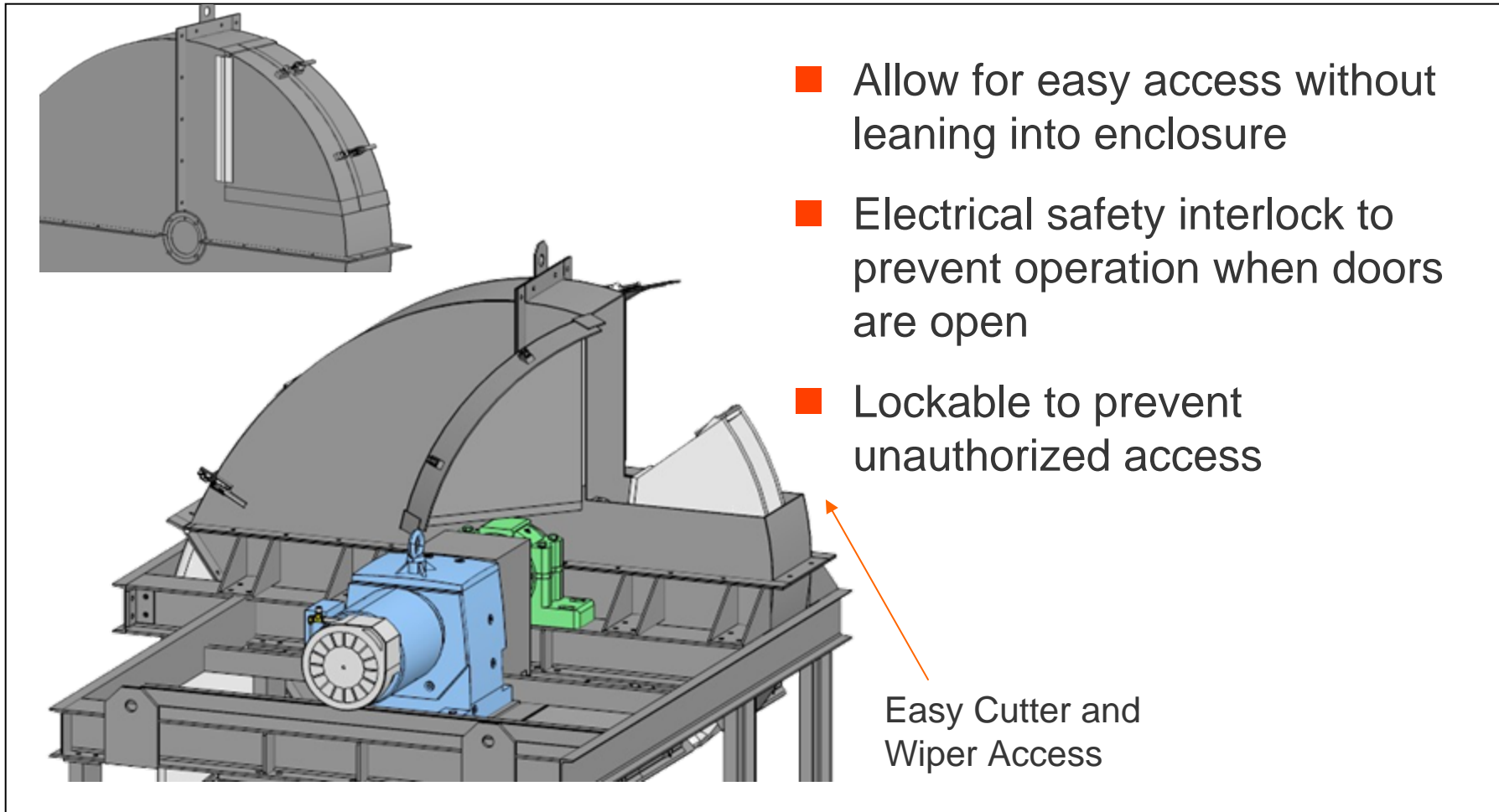




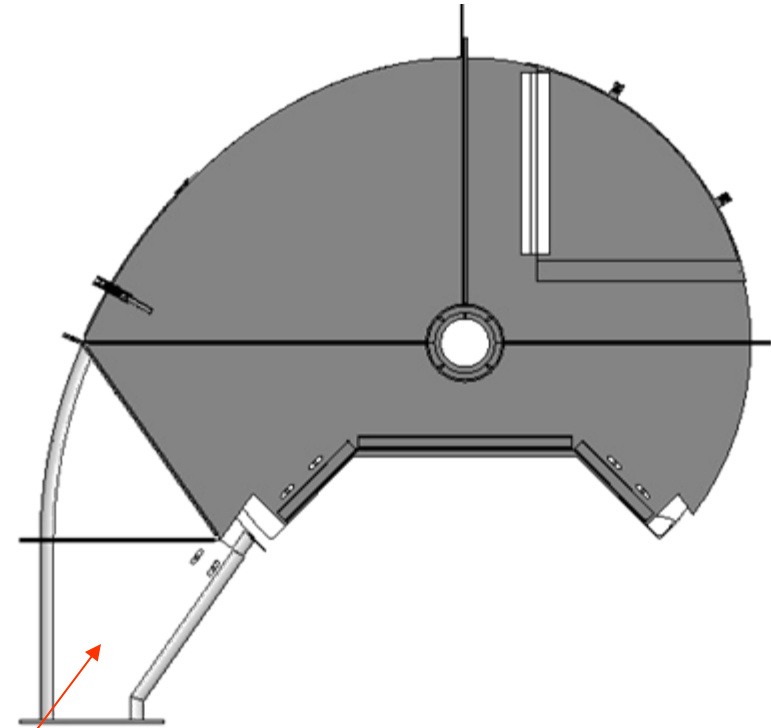
ADJUSTABLE SKIRT BOARDS AND STRIKER PLATES

- Collect all the increment, all the time
- Striker plates ensure only the material within the cutter is collected with the increment.
- Reduce bias, error, and dust
- No residual sample material left on belt
- Keep all non-sample material on the belt, eliminate spillage
- Conforms to ISO, ASTM and other international standards





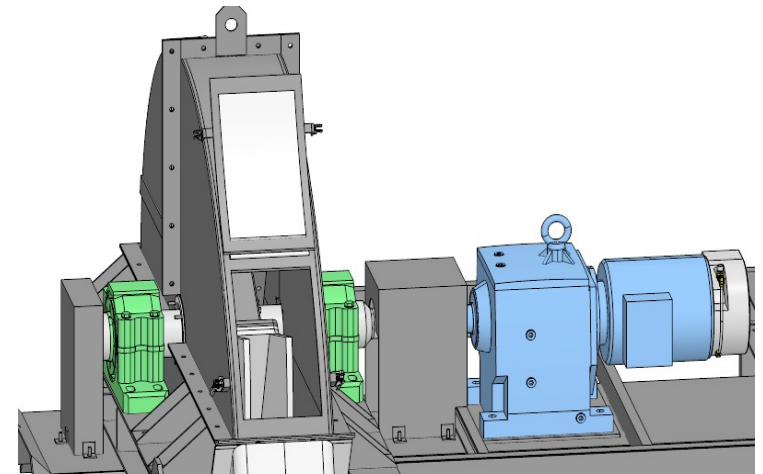
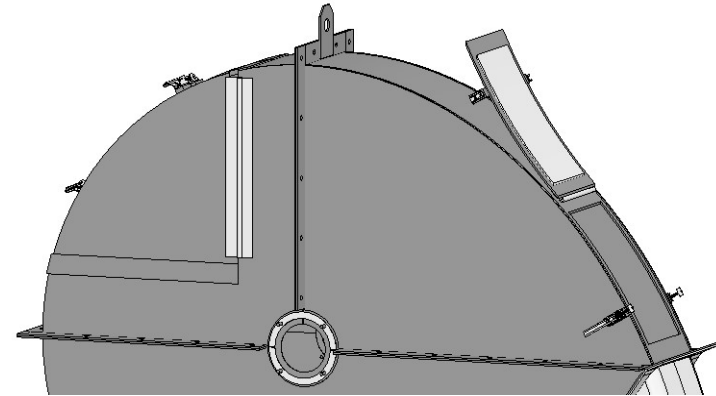
- Material impacts walls at 65° angle
- Prevents 'mushrooming' and sticking of sample on enclosure walls
- Maintains material velocity all the way to the discharge flange



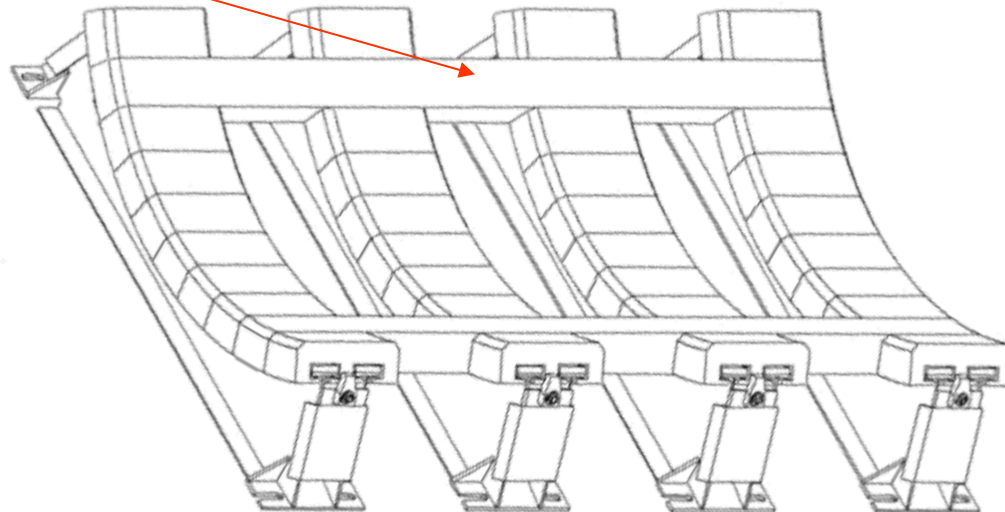
Fully Stainless Steel Chute
With 2" Radius Corners

CHUTE INSPECTION DOOR

- Easy chute or cutter access
- Lockable latches
- Inner liner to keep inside of enclosure as flat as possible, reducing places for material to stick

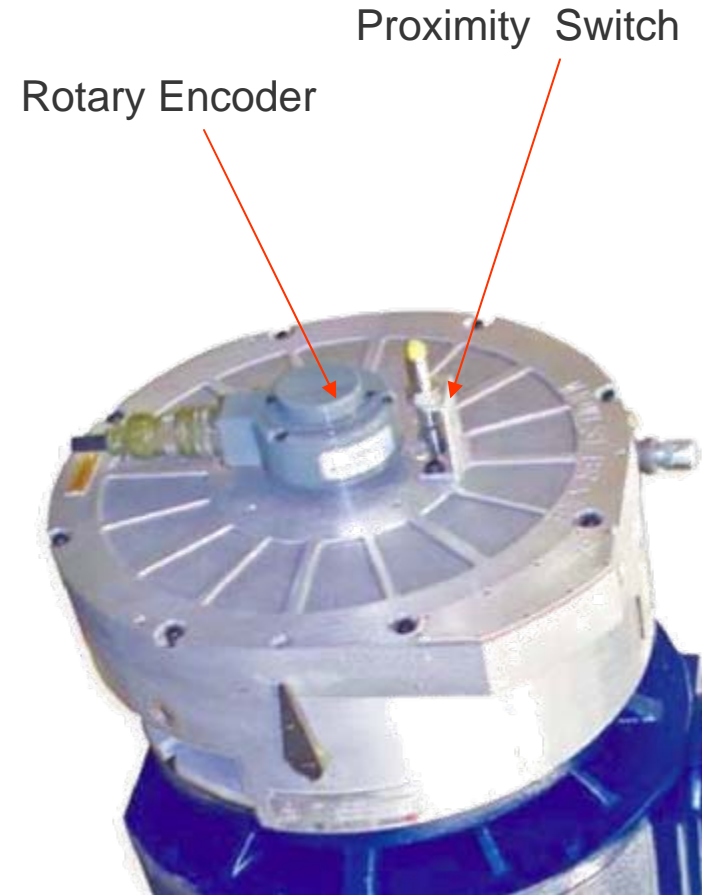


- Conforms belt perfectly to cutter trajectory (training idlers not shown)
- Ensures that no material is left behind by the cutter
- Extra protection along skirt boards to prevent material loss as spillage



OPTIONAL CLOSED LOOP SPEED AND POSITION CONTROL

- Shaft encoder integrated with fluid shear brake or hydraulic motor
 - Allows for real-time feedback to control software
 - Operational speed can be verified and an alarm can be triggered if the correct speed is not reached in the designated angle
 - Any slowing through material can be monitored and accounted for, an alarm can be triggered if conditions change out of nominal parameters
 - Dynamic acceleration and braking control reduces stress on components
 - Park position and acceleration/braking curves precisely defined and monitored, no 'timer based' motion control
 - No 'tuning' necessary once system is set up



OPTIONAL HYDRAULIC DRIVE

- Extreme duty drive
- Fully dynamic motion control
- Extreme torque and shock capacity
- 100% thermal control for full response in any environment
- Very low maintenance
- No need for a gearbox or separate brakes (holding brake and stopping brake included)
- Complete integrated solution
 - Motor
 - Power unit
 - Hydraulic controls
 - Hydraulic system health monitoring



OPTIONS TO MITIGATE HARSH ENVIRONMENT

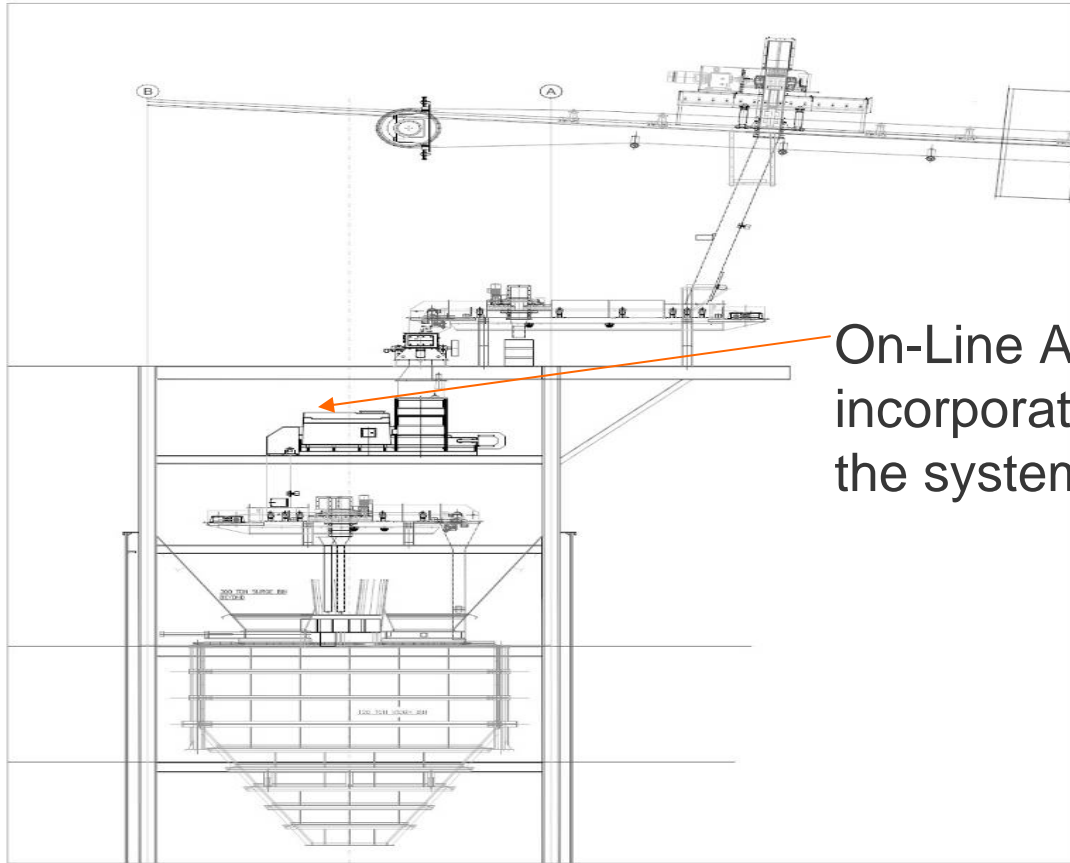
- Fully stainless steel systems
- Wash-down rated equipment
- Explosion proof electrics (Hazardous environment conditions)
- Epoxy coated components (Highly corrosive applications)
- Galvanized framework
- Stainless hardware

CROSS BELT SAMPLERS – DESIGN RULES

- Rule 1: The cutter aperture must travel at a 90 degree angle to the centerline of the belt being sampled.
- Rule 2: The cutter aperture width must be no less than three times the nominal top size of the material (3d).
- Rule 3: The arc formed from the leading edge to the trailing edge of the sidewalls must be sufficient for the cutter to cover the width of the material on the belt at full CEMA loading.
- Rule 4: The cutter must pass through the entire stream of material during one continuous operation with a minimum cutter velocity at the tip of the cutter near the belting of 1.5 times the velocity of the belt.
- Rule 5: Striker plates for prohibiting the entry of non-sample material must be installed on both the upstream and downstream sides of the cutter exit opening with gaps between the exiting cutter and striker plate held to no more than 10 mm.
- Rule 6: The underlying belting must be securely supported in such a way as to conform the belting to the cutter path (a circle).

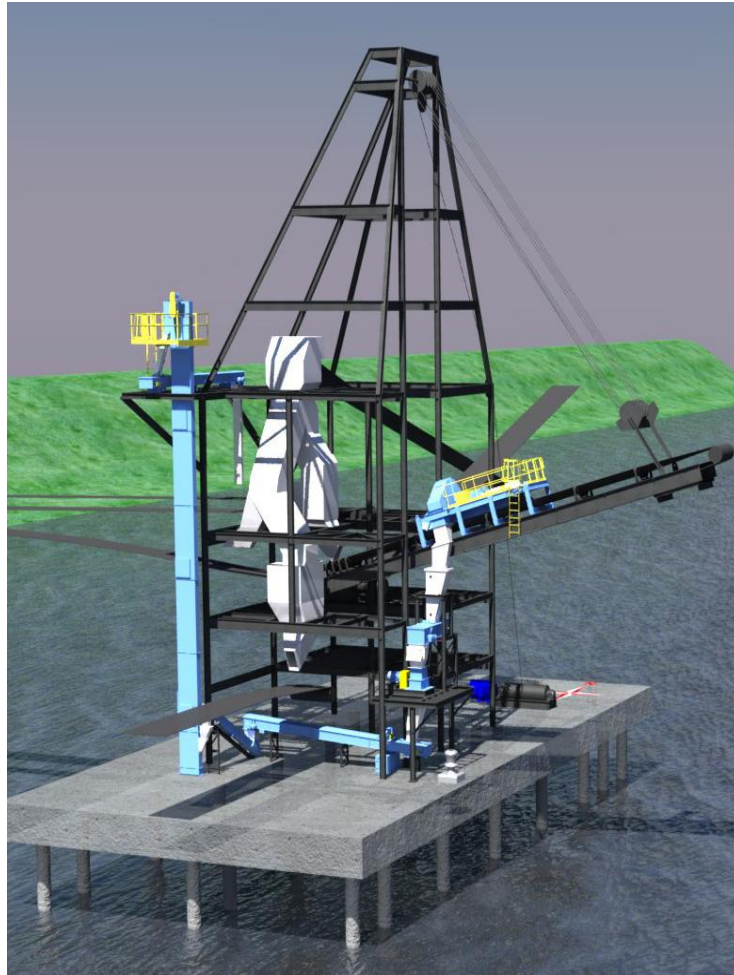
- Rule 7: The gap between the cutter side plates and the conveyor belting must not be greater than 10 mm at any point across the belt.
- Rule 8: The cutter must be equipped at the rear with an effective and durable wiper that cleanly scrapes the belting.
- Rule 9: The cutter must not be fitted with internal supports that could interfere with material entering or exiting the cutter.
- Rule 10: All cutters for belt sizes 900 mm and larger must be counterweighted. This avoids potential structural problems with the conveyor belt.
- Rule 11: All material delimited by the cutter and none other, must be included in the sample.
- Rule 12: No material shall remain in the cutter after the cutter has collected and discharged an increment. This is to be verified visually and by tests of the sampling ratio.

- Fully turn-key sampling systems
 - Samplers (Primary, Secondary, Tertiary)
 - Cross Belt
 - Falling Stream
 - Auger
 - Feed and Discharge Belts
 - All Chute work
 - Power, Instrumentation and Control Integration with Existing Systems



On-Line Analyzer
incorporated into
the system.

COMPLICATED INTEGRATION OF A MSS INTO AN EXISTING FACILITIES



- Primary sampler mounted on a loading boom that is raised and lowered.



OTHER SGS MECHANICAL SAMPLING SYSTEM SERVICES

- Bias Testing of Sample Systems
- Sampling System Inspection Services
- Engineering Studies to design and justify
- Field installation and Project management
- Integration of On-Line Analyzers into the system
- Operation and maintenance services

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WHEN YOU NEED TO BE SURE

